A second-order cut-cell method for the numerical simulation of 2D flows past obstacles

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Navier-Stokes equations for incompressible fluid flow

Given $\mathbf{x} \in \Omega \subset \mathbb{R}^2$ and t > 0. Velocity and pressure fields $\mathbf{u} = \mathbf{u}(\mathbf{x}, t) \in \mathbb{R}^2$, $p = p(\mathbf{x}, t) \in \mathbb{R}$ are solution of

 $\begin{aligned} &\partial_t \mathbf{u} + \operatorname{div} \left(\mathbf{u} \otimes \mathbf{u} \right) - \Delta \mathbf{u} / Re + \nabla p = \mathbf{f} \text{ in } \Omega, \\ &\operatorname{div} \mathbf{u} = 0 \text{ in } \Omega, \\ &\mathbf{u} = \mathbf{g} \text{ on } \partial \Omega, \\ &\mathbf{u} = \mathbf{u}_0 \text{ at } t = 0. \end{aligned}$

with

$$Re = U_*L_*/\nu_*$$

and

$$\nu = \mu / \rho$$
 kinematic viscosity.

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Backward F.D. scheme + Projection method (1/2)

Let $\delta t > 0$. Given $\mathbf{u}^k(\mathbf{x}) \approx \mathbf{u}(\mathbf{x}, t_k)$ and $p^k(\mathbf{x}) \approx p(\mathbf{x}, t_k)$, $t_k = k \delta t$,

we solve the prediction step :

$$\frac{3\tilde{\mathbf{u}}^{k+1} - 4\mathbf{u}^k + \mathbf{u}^{k-1}}{2\delta t} - \Delta \tilde{\mathbf{u}}^{k+1}/Re = -\nabla p^k + \mathbf{f}^{k+1}$$
$$-2 \operatorname{div}(\mathbf{u}^k \otimes \mathbf{u}^k) + \operatorname{div}(\mathbf{u}^{k-1} \otimes \mathbf{u}^{k-1}),$$
$$\tilde{\mathbf{u}}^{k+1}|_{\partial\Omega} = \mathbf{g}.$$

then the **projection step** :

$$\mathbf{u}^{k+1} = \tilde{\mathbf{u}}^{k+1} - 2\delta t \,\nabla (\delta p^{k+1})/3$$
$$\operatorname{div} \,\mathbf{u}^{k+1} = 0$$
$$\left(\mathbf{u}^{k+1} - \tilde{\mathbf{u}}^{k+1}\right)|_{\partial\Omega} \,.\mathbf{n} = 0.$$

with $\delta p^{k+1} = p^{k+1} - p^k$.

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Backward F.D. scheme + Projection method (2/2)

Pressure increment δp^{k+1} is solution of :

At each iteration,

- 1. solve prediction step,
- solve system on pressure increment,
- 3. correction of velocity via projection step.



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M.A.C. Scheme : position of unknowns Let $\Omega = (0, L) \times (0, H)$.

We consider $\ell = L/n_{\ell}$, $h = H/n_h$, $x_i = i \ell$ and $y_i = j h$.

 $K_{i,i} = [x_{i-1}, x_i] \times [y_{i-1}, y_i]$

$$u_{ij}(t) \simeq \langle u(.,t) \rangle_{K_{i+\frac{1}{2},j}}, \quad v_{ij}(t) \simeq \langle v(.,t) \rangle_{K_{i,j+\frac{1}{2}}},$$

 $p_{ij}(t) \simeq \langle p(.,t) \rangle_{K_{i,j}}, \quad \text{where} \quad \langle w \rangle_{K} = \frac{1}{|K|} \int_{K} w(\mathbf{x}) \, d\mathbf{x}$

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F H Harlow and 1 F Welch, Numerical calculation of timedependent viscous incompressible flow of fluid with free surface, Phys. Fluids 8, 1965.

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Immersed boundary methods on cartesian grid



simulation of flows in complex geometry

 in the literature, several methods exist : forcing, ghost cell, penalization, cut cell Fluid flows around obstacles 9/26

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Taking into account the obstacle

Rectangular domain Ω .

The obstacle Ω^S is bounded by a closed curve Γ .



Algebraic distance $d : \Omega \to \mathbb{R}$ is defined by :

$$d(\mathbf{x}) = \left\{ egin{array}{ll} \operatorname{dist}(\mathbf{x}, \Gamma) & ext{if } \mathbf{x} \in \Omega^S, \ & \ -\operatorname{dist}(\mathbf{x}, \Gamma) & ext{otherwise.} \end{array}
ight.$$

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Cell-face ratio



 x_{i-1}

O. Botella and Y. Cheny, *The LS-STAG method: A new immersed* boundary/level-set method for the computation of incompressible viscous flows in complex moving geometries with good conservation properties, J. Comp. Phys. **229**, 2010.

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 x_i

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Position of unknows



Position of velocity field well-adapted to divergence

Interpolation of the pressure gradient

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Far away from the obstacle : second order centered discretization

Near the obstacle :

 $\begin{cases} \triangle \mathbf{u} : \text{ first order Finite Difference approximation} \\ \text{div}(\mathbf{u} \otimes \mathbf{u}) : \text{ first order Finite Volume approximation} \end{cases}$

N. Matsunaga and T. Yamamoto, *Superconvergence* of the Shortley-Weller approximation for Dirichlet problems, J. Comp. Appl. Math. **116**, 2000.



Second order accurate Fluid flows around obstacles 13/26

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Discretization of the prediction step : $\triangle u$

First-order Finite Difference approximation is exact on $\mathbb{R}_2[X, Y]$.

 $\mathcal{V} = \{O, N, S, E, W, P\}$

- ▶ *O* the position of *u*_{*ij*},
- N, S, E, W among unknowns close to O or on the board Γ,
- P arbitrarily chosen



Find coefficients α_M such that :

$$\sum_{M\in\mathcal{V}}\alpha_M u(M) = \bigtriangleup u(O) + \mathcal{O}(h).$$

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Discretization of the prediction step : div $(\mathbf{u} \otimes \mathbf{u})$





$$\begin{aligned} \bar{f}_{i,j} &= \int_{\tilde{K}_{i+\frac{1}{2},j}} \left(\partial_x (u^2) + \partial_y (uv) \right) \, d\mathbf{x} \\ &= \int_{\partial \tilde{K}_{i+\frac{1}{2},j}} \left(u^2 n_x + (uv) n_y \right) \, dS \\ &= F_{i+1,j}^E - F_{i,j}^E + F_{i,j}^N - F_{i,j-1}^N + F_{i,j}^B. \end{aligned}$$

 \rightarrow flux reconstruction

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Discretization of the correction step

- div u : Discrete divergence on cut cells
- ∇p : Interpolation of the pressure gradient

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Discretization of the correction step : div \mathbf{u} (1/2)

$$\iint_{\widetilde{K}_{i,j}} \operatorname{div} \mathbf{u} \, d\mathbf{x} = \int_{\partial \widetilde{K}_{i,j}} \mathbf{u}.\mathbf{n} \, dS$$
$$= \int_{\sigma_{i,j}^{u} \cap \Omega^{F}} u dS - \int_{\sigma_{i-1,j}^{u} \cap \Omega^{F}} u \, dS$$
$$+ \int_{\sigma_{i,j}^{v} \cap \Omega^{F}} v dS - \int_{\sigma_{i,j-1}^{v} \cap \Omega^{F}} v \, dS + \int_{\widehat{AB}} \mathbf{u}.\mathbf{n} \, dS,$$

with
$$\widehat{AB} = \Gamma \cap K_{i,j}$$
.



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Discretization of the correction step : div \mathbf{u} (2/2)



•
$$\int_{\sigma_{i,j}^u \cap \Omega^F} u \, dS \approx r_{i,j}^u \, h \, u_{i,j}$$
 and $\int_{\sigma_{i,j}^v \cap \Omega^F} v \, dS \approx r_{i,j}^v \, h \, v_{i,j}.$

$$(D_{obs}\mathbf{u})_{i,j} = h (r_{i,j}^{u}u_{i,j} - r_{i-1,j}^{u}u_{i-1,j}) + h (r_{i,j}^{v}v_{i,j} - r_{i,j-1}^{v}v_{i,j-1}) + L \mathbf{g} ((A + B)/2) \cdot \mathbf{n}_{i,j} = (D_{obs}^{0}\mathbf{u})_{i,j} + D_{i,j}^{supp}$$

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Discretization of the correction step : $\mathcal{P}_{\phi}G\delta p$

$Gp = \left(\begin{array}{c} (p_{i+1,j} - p_{i,j})/h \\ (p_{i,j+1} - p_{i,j})/h \end{array}\right)$

Without



$$D(G\delta p) = \frac{3}{2} \frac{h^2}{\delta t} D(\tilde{\mathbf{u}})$$

$$\Rightarrow \mathbf{u} = \tilde{\mathbf{u}} - \frac{2}{3} \frac{\delta t}{h^2} G\delta p$$

$$\Rightarrow D(\mathbf{u}) = 0$$

With



$$D_{obs}^{0}(\mathcal{P}_{\phi}(G\delta p)) = \frac{3}{2} \frac{h^{2}}{\delta t} D_{obs}(\tilde{\mathbf{u}})$$

$$\Rightarrow \mathbf{u} = \tilde{\mathbf{u}} - \frac{2}{3} \frac{\delta t}{h^{2}} \mathcal{P}_{\phi}(G\delta p)$$

$$\Rightarrow D_{obs}(\mathbf{u}) = 0$$

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Solver

 $\mathsf{Obstacle} \to \textbf{nonsymmetric} \text{ linear system}$

• Iterative methods for solving linear systems Cut cells \rightarrow ill-conditioned linear systems \rightarrow slow convergence \rightarrow simulation on coarse mesh \rightarrow simulations of flow at moderate Reynolds

Direct method for solving linear systems

Unmoving obstacle :

- Preprocessing step : O(n³) operations, once per simulation.
- Every iteration : O (n²logn) operations (idem without obstacle).

B.L. Buzbee, F.W.Dorr, J.A. George and G.H. Golub, *The direct* solution of the discrete Poisson equation on irregular regions, J. Num. Anal. **8**, 1971. Fluid flows around obstacles 20/26

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Numerical results : Re = 40Laminar flows



$$\sum \text{Forces}_{/\text{obstacle}} = \frac{1}{2} \rho A u_{\infty} \begin{pmatrix} C_d \\ C_l \end{pmatrix}$$

Re = 40				
C _d	θ	1	а	b
	53.8	2.13	0.76	0.59
1.62	54.2	2.18		
1.52	53.8	2.35		
1.50	55.6	2.24		
1.54	53.6	2.28	0.72	0.60
1.55	54.1		0.73	0.60
1.50	53.4	2.26	0.710	0.60
	C _d 1.62 1.52 1.50 1.54 1.55 1.50	$\begin{array}{c c} & \\ \hline C_d & \\ & 53.8 \\ 1.62 & 54.2 \\ 1.52 & 53.8 \\ 1.50 & 55.6 \\ 1.54 & 53.6 \\ 1.55 & 54.1 \\ 1.50 & 53.4 \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

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Numerical results : Re = 9500

 $\Omega = (-5,5) \times (-2.5,2.5)$, obstacle = disk, D = 1Non-uniform grid, 3072 mesh points in each direction Near the obstacle $h = 1.6 \ 10^{-3}$ CFL stability condition $\Rightarrow \delta t = 10^{-4}$



Figure: Evolution of the boundary layer : comparison with experimental results.

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Numerical results : flow past a NACA airfoil





Figure: Flow behind NACA 0012 at Re = 1 000, incidence 34° : comparison with experimental results

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Conclusion and prospects

Accurate (second order) and fast (efficient solver) new cut cell method.



- 1. Three Dimensional flows
- 2. Coupling with :
 - H-box method (avoid the small cell problem, $\delta t \nearrow$)
 - Turbulence model (flows at high Re)
 - Local grid refinement
 - Domain decomposition

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